Foans: Microstructural Design - feams - behaviour dominated by cell wall bending . foan properties can be increased by increasing EI of cell walls Hollow walls

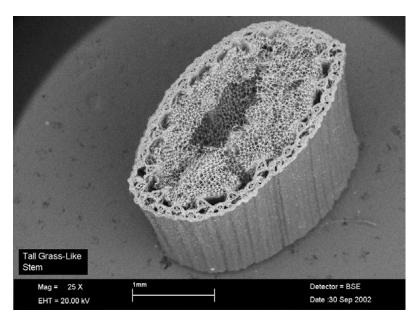


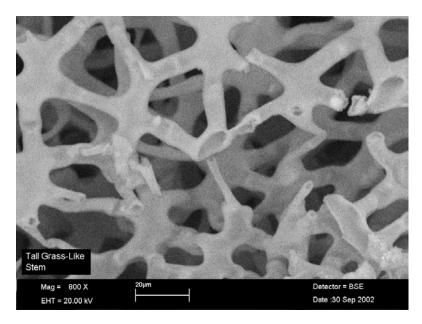
thin walled tube $I_{t} = \pi r^{3}t$ Masses equal: $\pi R^{2} = 2\pi rt$ Solid circular section $I_{s} = \frac{\pi R^{4}}{4}$ $R = \sqrt{2}rt$

$$\frac{I_{t}}{I_{s}} = \frac{4 \pi r^{3} t}{\pi r^{4}} = \frac{4 r^{3} t}{4 r^{2} t^{2}} = \frac{r}{t}$$

· can do similar analysis for other properties







Sandwich cell walls

- d= form cell size

Microsandwich foan

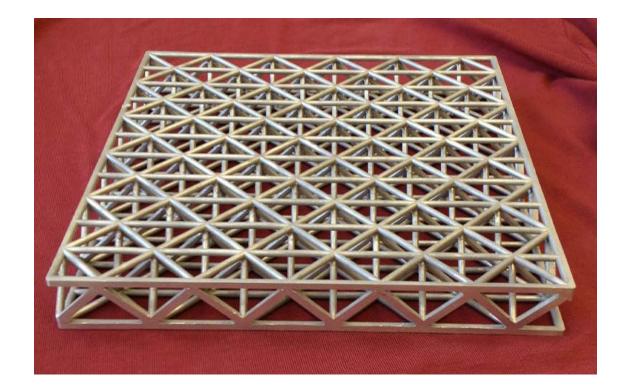
- thin walled hollow spheres distributed in a form
- · have to get geometry right
- · require :

Spheres: t << D Esphere >> Efoam Vf spheres 2 50-60% foan: d << c

Foams: Microstructural design

- · another alternative is to use microstructure that induces axial, rather than bending, deformations
- · 3D lattice materials triangulated trusks in 3D - forces in members all axial; bending negligible
- · Various processing methods + geometries possible all triangulated
- · can analyze truss as having pin joints axial forces in members
- · open cell structures

$$E^{*} = \underbrace{\mathcal{G}}_{E} \propto \underbrace{F}_{A^{2}} \frac{1}{S} \qquad \underbrace{\mathcal{S}}_{A} \xrightarrow{FI}_{AE_{s}} \propto \underbrace{FI}_{A^{2}E_{s}} \\ E^{*} \propto \underbrace{F}_{A} \underbrace{E_{s}t^{2}}_{FA} \propto \underbrace{E_{s}(\frac{t}{e})^{2}}_{A} \propto \underbrace{E_{s}(\rho^{*})}_{\rho_{s}} \\ \boxed{E^{*} = C E_{s}(\rho^{*}|\rho_{s})} \qquad C \text{ depends on cell geometry } + \text{ loading direction} \\ \text{Strength}: if struts fail by uniaxic1 yett \\ \mathcal{G}_{p}^{*} = C \mathcal{G}_{ys}(\rho^{*}|\rho_{s}) \\ \underbrace{B_{u}\Gamma}_{some struts in Compression - may buckle}(\text{generally do buckle}) \end{aligned}$$



Compressive strut buckling

- · elastic buckling Jei = CEs (p*/ps)2 (like an open-cell form)
- · if interaction between ebstic buckling + yield use a reduced modulus (tangent modulus)
- · also: imperfections such as non-staight strats

 - or misaligned struts reduce buckling resistance "knock-down" factor can be significant ~ 502.

Material selection

- how to select the test material for some mechanical requirement?
 section on wood: derived performance index for minimizing mass of a team of a given stiffness: E'21p
 - · here, Liscuss materials selection more broadly
 - · another example: What material minimizes the mass of a bean of a given failure load, Pf? given Pf, span l, square coss-section t²
 - $\begin{aligned}
 \overline{\sigma}_{max} &= \frac{My}{T} \\
 \overline{\sigma}_{max} & \frac{P_{f} l t}{t^{4}} \neq \sigma_{f} \\
 t & \frac{P_{f} l}{t^{4}} \end{pmatrix}^{1/3} \\
 \overline{\sigma}_{f} \\
 \hline{\sigma}_{f} \\
 mass, m = p t^{2} l \\
 m & p \left(\frac{P_{f} l}{\sigma_{f}}\right)^{2/3} l
 \end{aligned}$
- M= Maximum moment in bean & Pl y = mourimum distance from neutral axis & t I = moment of metria & t⁴ Of = failure stress of bean material

Performance index: 57²¹³/p to be maximized

Materials selection

Ashby book -	· can obtain performance indices for various loading configurations +
	mechanical requirements
Table	· if plot data for material properties an log-log scales, performance
	indices appear as straight lines
	· shifting lines up + down identifies best material for that performance
CHNM	example: midulus - density chart
Fig 7.1	Elp: axially loaded tie of given stiffness
	E'2/p: bean of given stiffness
	E'slp: plate " "

Property charts for forms E* vs p* : range of E* factor of 10°, from 0.01 MPa to 10GPa CS Fig 13.1 ot vs pt : range of ot from 10-3 to 30 MPa Fig 13.2 => scope for matching formi properties to design requirements E*/p vs o*/p : end grain balsa, metal foans high values nseful for sand with panels - selection of cove makinal Property charts - forms

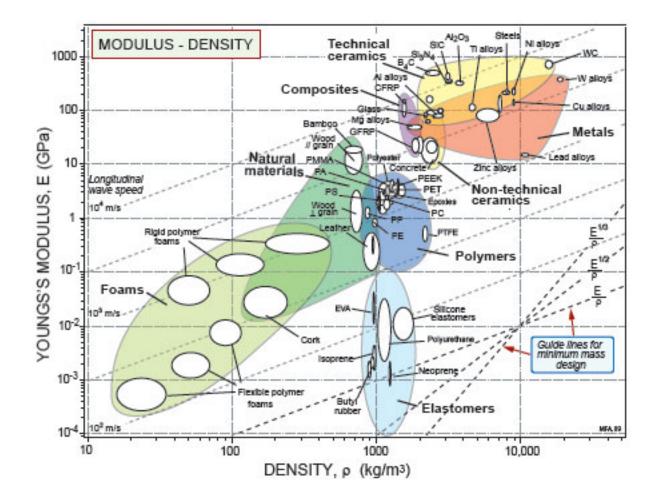
Ep vs. $\sigma_{25^{\prime}}^{*}$: contours show energy absorption/volume, \mathcal{U} $\mathcal{U} \sim \sigma_{25^{\prime}}^{*}$. Ep $\sigma_{25^{\prime}}^{*}$. $\overline{\mathcal{U}}_{1111111}^{*}$ = ε_{0} $\varepsilon_{0} = \mathcal{U}/\sigma_{25^{\prime}}^{*}$. $\overline{\mathcal{U}}_{50}^{*}$. $\overline{\mathcal{U}}_{50}^{*}$ = ε_{0} contours have slope of -1 an log-log scales balea, metal focus - high values of \mathcal{U}

- · can also produce selection charts for other properties e.g. thermal
- λ vs σ^{*}_{sr} thermal conductivity, λ - thermal insulation applications usually have constraint on strength, too.
- · I vs Tmax may have constraint an maximum service temprative, to.
- · density plot closed cell forms buoyancy
- · cell size open cell france filhation + catalysis
 - Surface area /when in creases as cell size decreases e.g. Ceramic forms used in filtration of liquid metals

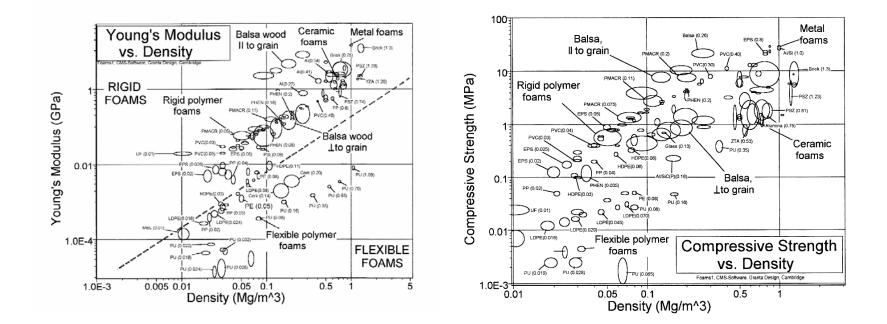
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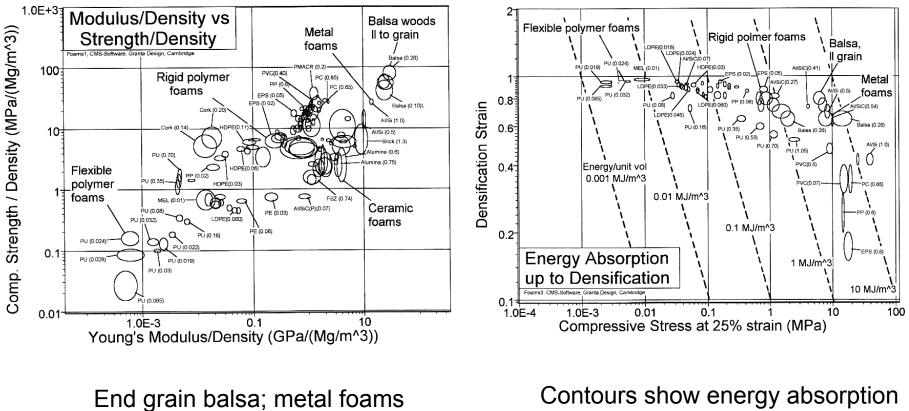
Ashby MF (1999) Materials Selection in Mechanical Design. Second Edition Butterworth Heinemann



Ashby plot of Young's Modulus - Density © Granta Design. All rights reserved. This content is excluded from our Creative Commons license. For more information, see http://ocw.mit.edu/help/faq-fair-use/.



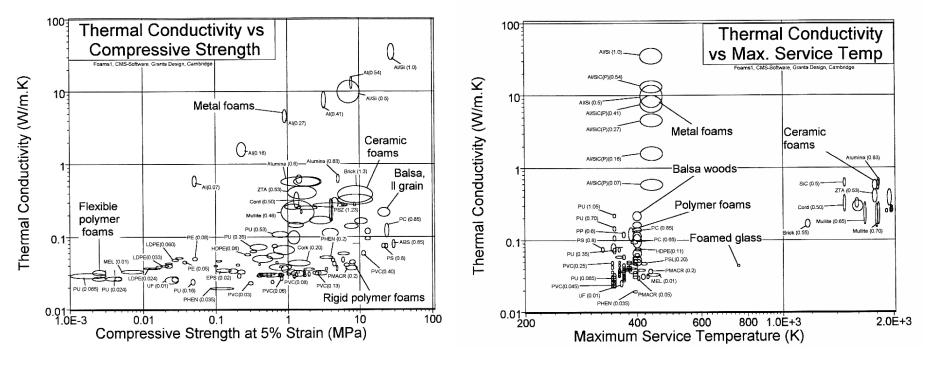
Gibson, L. J., and M. F. Ashby. *Cellular Solids: Structure and Properties*. 2nd ed. Cambridge University Press, © 1997. Figures courtesy of Lorna Gibson and Cambridge University Press.



Useful for sandwich panels

Contours show energy absorption per unit volume

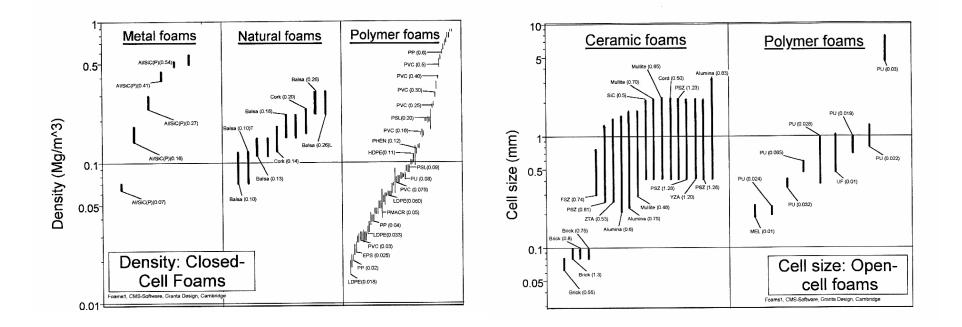
Gibson, L. J., and M. F. Ashby. Cellular Solids: Structure and Properties. 2nd ed. Cambridge University Press, © 1997. Figures courtesy of Lorna Gibson and Cambridge University Press.



Thermal insulation applications; Usually a constraint on strength, too

May also have a constraint on maximum service temperature

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Buoyancy

Filtration and catalysis

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