

# Lecture 8 Foam Design Notes, 3.054

## Foams: Microstructural Design

- Foam—behavior dominated by cell wall bending
- Foam properties can be increased by increasing EI of cell walls

### Hollow walls



Thin walled tube  $I_t = \pi r^3 t$

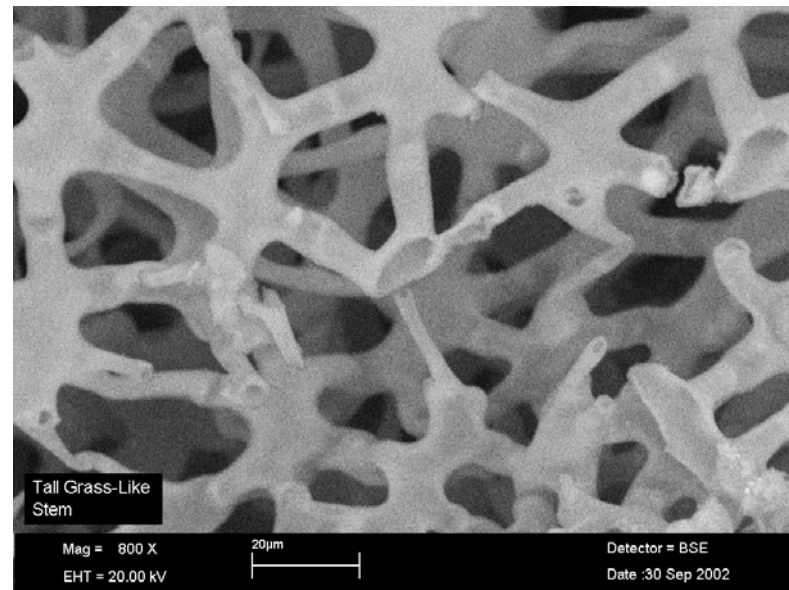
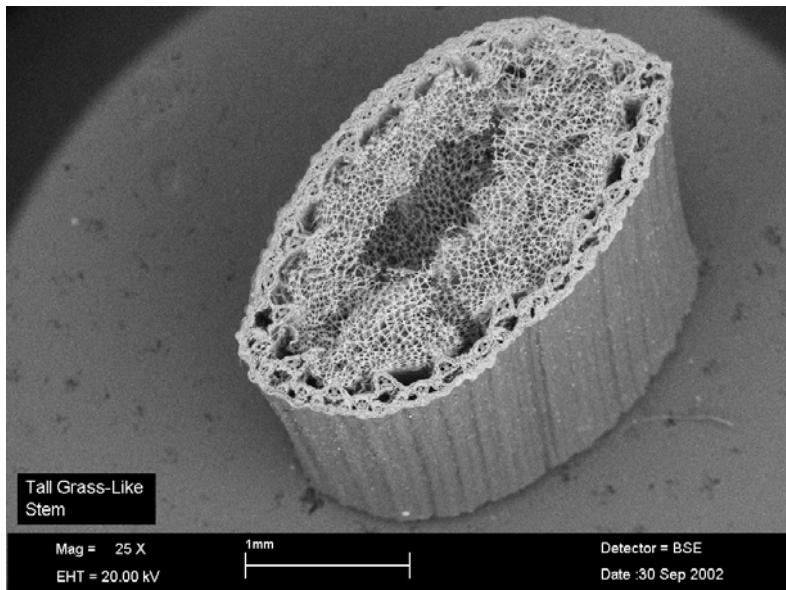
Solid circular section  $I_s = \frac{\pi R^4}{4}$

$$\begin{aligned} \text{Masses equal: } \pi R^2 &= 2\pi r t \\ R &= \sqrt{2rt} \end{aligned}$$

$$\frac{I_t}{I_s} = \frac{4\pi r^3 t}{\pi R^4} = \frac{4r^3 t}{4r^2 t^2} = \frac{r}{t}$$

$$\therefore \frac{E_{\text{tube wall}}^*}{E_{\text{solid wall}}^*} \propto \frac{r}{t}$$

- Can do similar analysis for other properties



## Sandwich cell walls

- Sandwich beam — two stiff faces separated by a lightweight core
  - core typically a honeycomb or foam (or balsa)



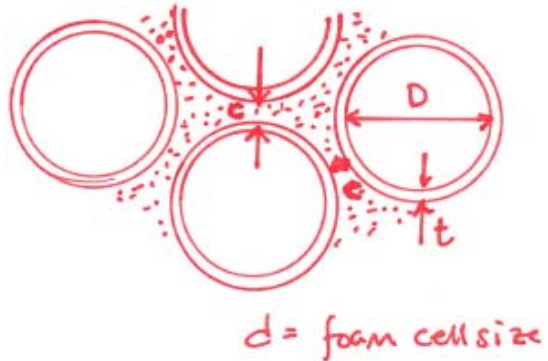
I-beam effect - increase in moment of inertia, with little increase in weight

Faces — like flanges of I-beam — resist bending

Core — like web of I-beam — resist shear

- Microsandwich foam

## Microsandwich foam



- Thin walled hollow spheres distributed in a foam
- Have to get geometry right
- Require:

Spheres:  $t \ll D$

$E_{\text{sphere}} \gg E_{\text{foam}}$

$V_{\text{f sphere}} \approx 50 - 60\%$

Foam:  $d \ll c$

## Foams: Microstructural Design

- Another alternative is to use microstructure that induces axial, rather than bending, deformations
- 3D lattice materials: — triangulated trusses in 3D  
— Forces in members all axial; bending negligible
- Various processing methods and geometries possible - all triangulated
- Can analyze truss as having pin joints - axial forces in members
- Open-cell structures

$$E^* = \frac{\sigma}{\epsilon} \propto \frac{F}{l^2} \frac{l}{\delta} \quad \delta \propto \frac{Fl}{AE_s} \propto \frac{Fl}{t^2 E_s}$$

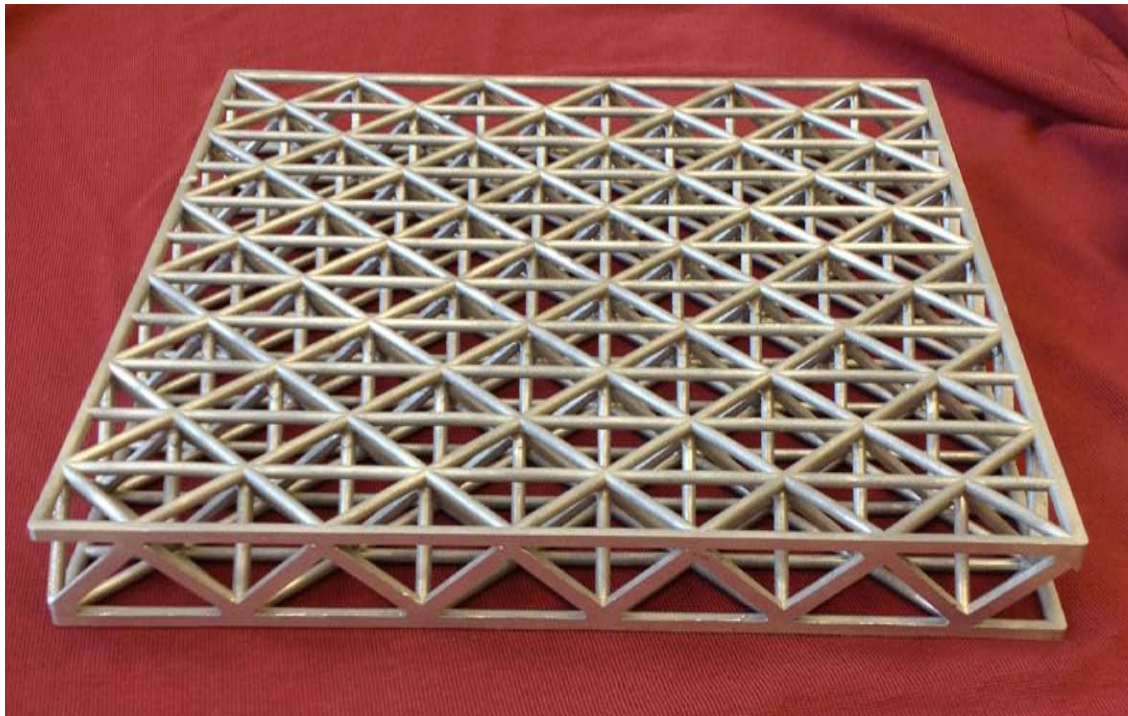
$$E^* \propto \frac{F}{l} \frac{E_s t^2}{Fl} \propto E_s \left(\frac{t}{l}\right)^2 \propto E_s \left(\frac{\rho^*}{\rho_s}\right)$$

$$\boxed{E^* = C E_s (\rho^* / \rho_s)} \quad C \text{ depends on cell geometry and loading direction}$$

- Strength: if struts fail by *uniaxial yield*:

$$\sigma_{pl}^* = C \sigma_{ys} (\rho^* / \rho_s)$$

*But* some struts in compression - may *buckle* (generally do buckle)



## Compressive strut buckling

- Elastic buckling  $\sigma_{el}^* = CE_s (\rho^*/\rho_s)^2$  (like open-cell foam)
- If interaction between elastic buckling and yield — use a reduced modulus  
(tangent modulus)
- Also: Imperfections such as non-straight struts or misaligned struts  
reduce buckling resistance  
“knock-down” factor can be significant  $\sim 50\%$

## Material Selection

- How to select the best material for same mechanical requirement?
- Section on wood: derived performance index for minimizing mass of a beam of a given stiffness:  $E^{1/2}/\rho$
- Here, discuss material selection more broadly
- Another example: What material minimizes the mass of a beam of a given failure load,  $P_f$ ?  
Given  $P_f$ , span  $l$ , square cross-section  $t^2$

$$\sigma_{max} = \frac{M y}{I}$$

$$\sigma_{max} \propto \frac{P_f l t}{t^4} \propto \sigma_f$$

$$t \propto \left( \frac{P_f l}{\sigma_f} \right)^{1/3}$$

$M$  = maximum moment in beam  $\propto Pl$

$y$  = maximum distance from neutral axis  $\propto t$

$I$  = moment of inertia  $\propto t^4$

$\sigma_f$  = failure stress of beam material

Mass,  $m = \rho t^2 l$

$$m \propto \rho \left( \frac{P_f l}{\sigma_f} \right)^{2/3} l$$

Performing index:  $\sigma_f^{2/3}/\rho$   
to be maximized

## Material Selection

- Ashby book-Tables
- Can obtain performance indices for various loading configurations and mechanical requirements
  - If plot data for material properties on log-log scales, performance indices appear as straight lines
  - Shifting lines up and down identifies best material for that performance index
  - Example: modulus-density chart

CMNM  
Fig.7.1

$E/\rho$ : axially loaded tie of given stiffness

$E^{1/2}/\rho$ : beam of given stiffness

$E^{1/3}/\rho$ : plate of given stiffness

## Property charts for foams:

$E^*$  vs  $\rho^*$ : range of  $E^*$  factor of  $10^6$ , from 0.01 MPa to 10 GPa

$\sigma^*$  vs  $\rho^*$ : range of  $\sigma^*$  from  $10^{-3}$  to 30 MPa

→ scope for matching foam properties to design requirements

CS  
Fig.13.1  
Fig.13.2

$E^*/\rho$  vs  $\sigma^*/\rho$ : end grain balsa, metal foam high values

useful for sandwich panels - selection of core material

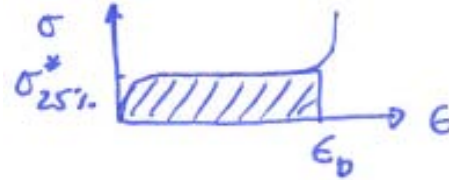


## Property charts for foams

$\epsilon_D$  vs  $\sigma_{25\%}^*$ : contours show energy absorption/volume,  $U$

$$U \sim \sigma_{25\%}^* \epsilon_D$$

$$\epsilon_D = U / \sigma_{25\%}^*$$



Contours have slope of  $-1$  on log-log scales  
Balsa, metal foams - high values of  $U$

- Can also produce selection charts for other properties — e.g. thermal
- $\lambda$  vs  $\sigma_{5\%}^*$  — thermal conductivity,  $\lambda$   
— thermal insulation applications usually have constraint on strength, too
- $\lambda$  vs  $T_{\max}$  — may have constraint on maximum service temperature, too
- Density plot — closed cell foams — buoyancy
- Cell size — open cell foams - filtration and catalysts  
— surface area/volume increases as cell size decreases  
e.g. ceramic foams used in filtration of liquid metals

Table removed due to copyright restrictions. See Table B1: Ashby, M. F. *Materials Selection in Mechanical Design*. 2nd ed. Butterworth Heinemann, 1999.

Ashby MF (1999) *Materials Selection in Mechanical Design*.  
Second Edition Butterworth Heinemann

**Table B2** Strength-limited design at minimum mass (cost, energy, environmental impact\*)

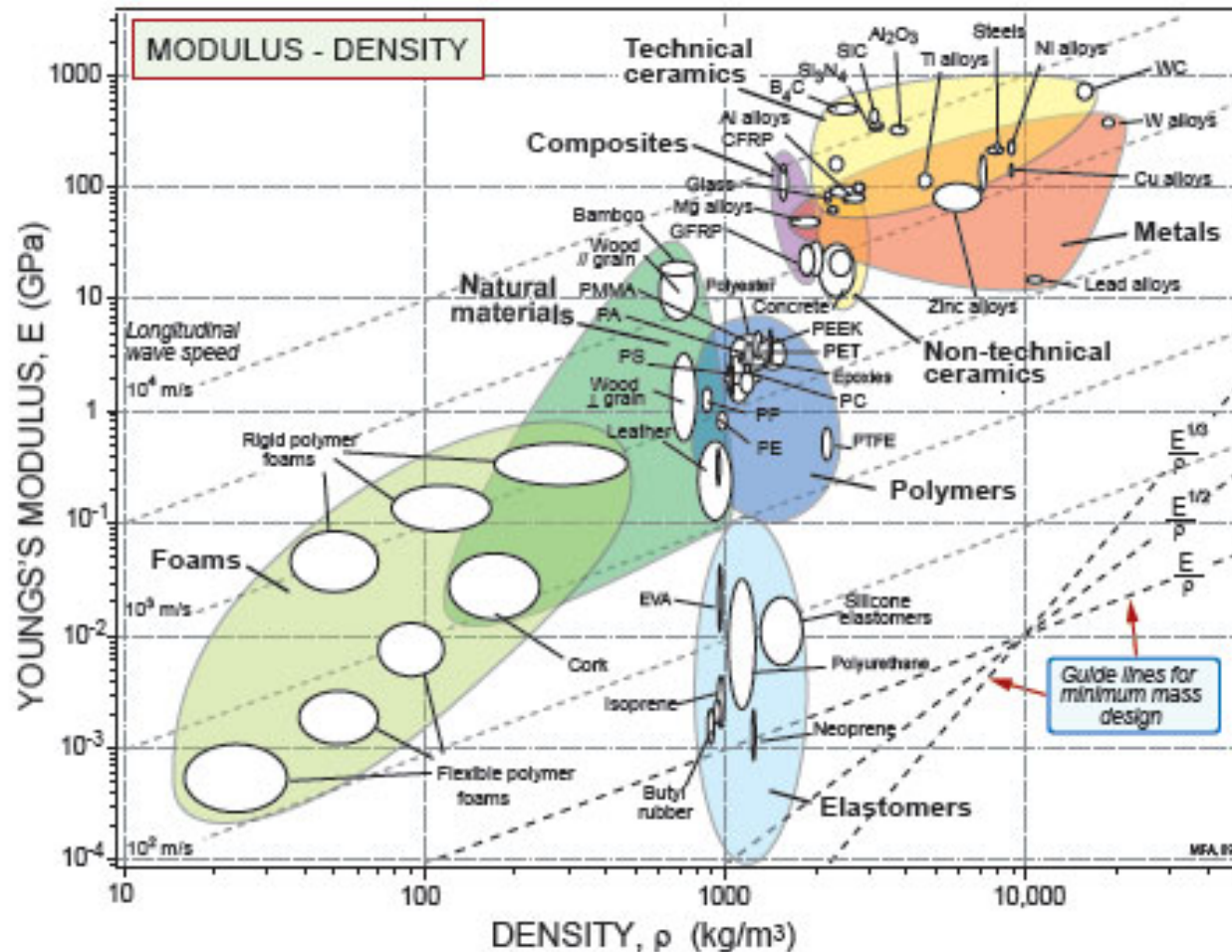
Function and constraints <sup>‡</sup>	Maximize <sup>†</sup>
<b>Tie (tensile strut)</b> stiffness, length specified; section area free	$\sigma_f / \rho$
<b>Shaft (loaded in torsion)</b> load, length, shape specified, section area free	$\sigma_f^{2/3} / \rho$
load, length, outer radius specified; wall thickness free	$\sigma_f / \rho$
load, length, wall-thickness specified; outer radius free	$\sigma_f^{1/2} / \rho$
<b>Beam (loaded in bending)</b> load, length, shape specified; section area free	$\sigma_f^{2/3} / \rho$
load length, height specified; width free	$\sigma_f / \rho$
load, length, width specified; height free	$\sigma_f^{1/2} / \rho$
<b>Column (compression strut)</b> load, length, shape specified; section area free	$\sigma_f / \rho$
<b>Panel (flat plate, loaded in bending)</b> stiffness, length, width specified, thickness free	$\sigma_f^{1/2} / \rho$
<b>Plate (flat plate, compressed in-plane, buckling failure)</b> collapse load, length and width specified, thickness free	$\sigma_f^{1/2} / \rho$
<b>Cylinder with internal pressure</b> elastic distortion, pressure and radius specified; wall thickness free	$\sigma_f / \rho$
<b>Spherical shell with internal pressure</b> elastic distortion, pressure and radius specified, wall thickness free	$\sigma_f / \rho$
<b>Flywheels, rotating discs</b> maximum energy storage per unit volume; given velocity	$\rho$
maximum energy storage per unit mass; no failure	$\sigma_f / \rho$

\*To minimize cost, use the above criteria for minimum weight, replacing density  $\rho$  by  $C_m \rho$ , where  $C_m$  is the material cost per kg. To minimize energy content, use the above criteria for minimum weight replacing density  $\rho$  by  $q\rho$  where  $q$  is the energy content per kg. To minimize environmental impact, replace density  $\rho$  by  $I_e \rho$  instead, where  $I_e$  is the eco-indicator value for the material (references [1] and [4]).

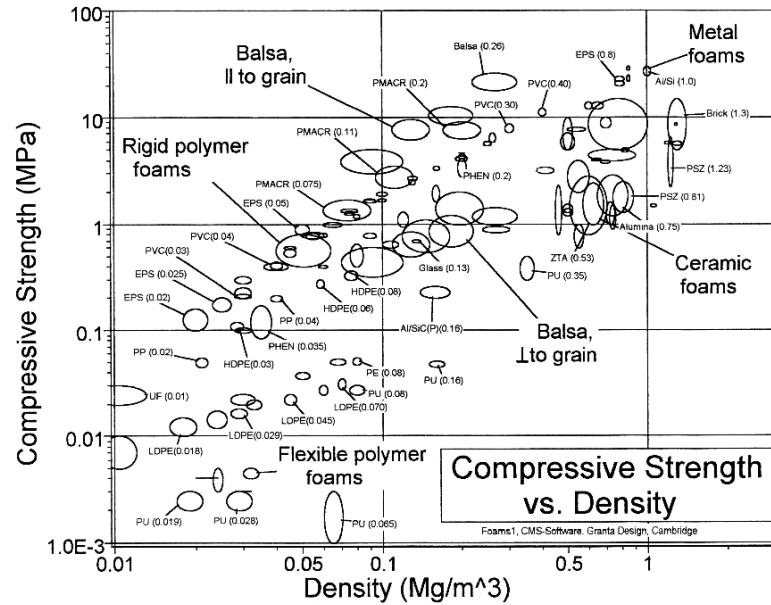
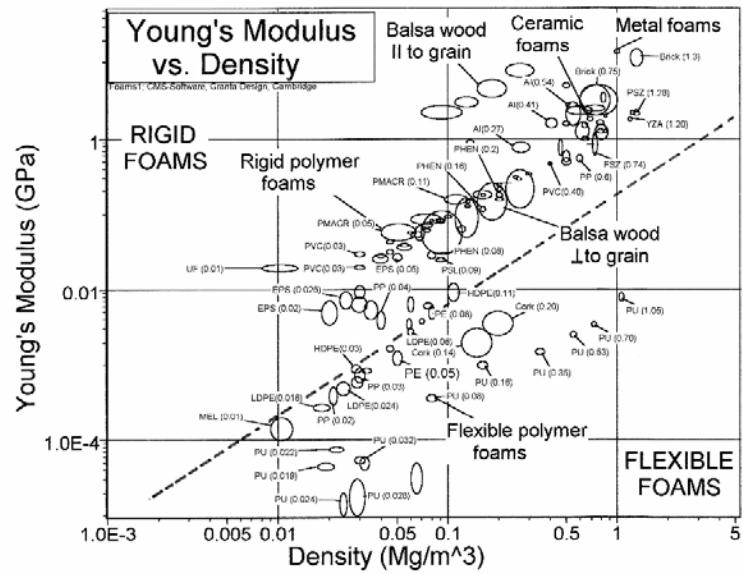
<sup>†</sup> $\sigma_f$  = failure strength (the yield strength for metals and ductile polymers, the tensile strength for ceramics, glasses and brittle polymers loaded in tension; the flexural strength or modulus of rupture for materials loaded in bending);  $\rho$  = density.

<sup>‡</sup>For design for infinite fatigue life, replace  $\sigma_f$  by the endurance limit  $\sigma_e$ .

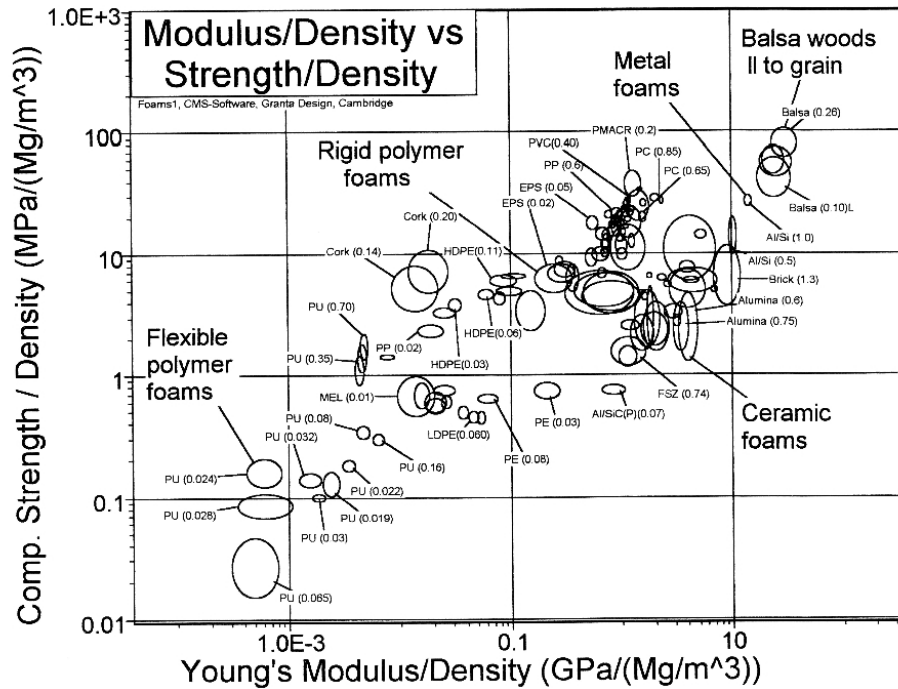
Ashby MF (1999) Materials Selection in Mechanical Design.  
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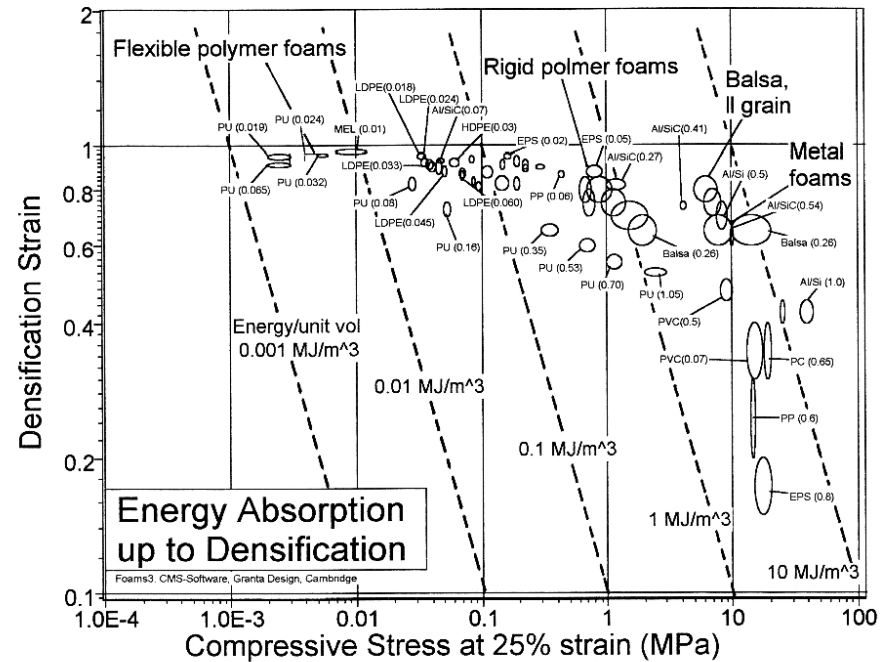
Ashby plot of Young's Modulus - Density © Granta Design. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <http://ocw.mit.edu/help/faq-fair-use/>.



Gibson, L. J., and M. F. Ashby. *Cellular Solids: Structure and Properties*. 2nd ed. Cambridge University Press, © 1997. Figures courtesy of Lorna Gibson and Cambridge University Press.

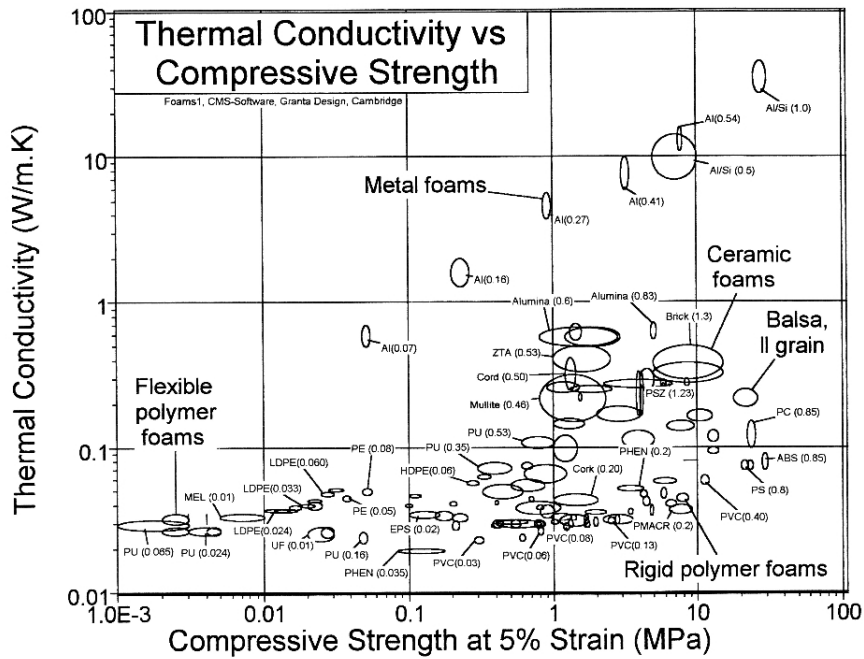


End grain balsa; metal foams  
Useful for sandwich panels

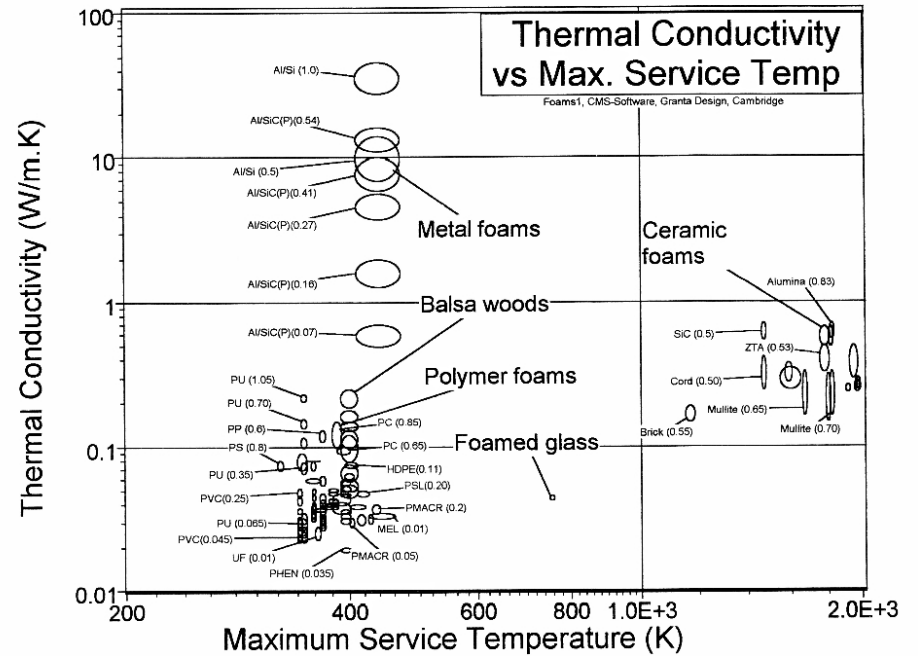


Contours show energy absorption  
per unit volume

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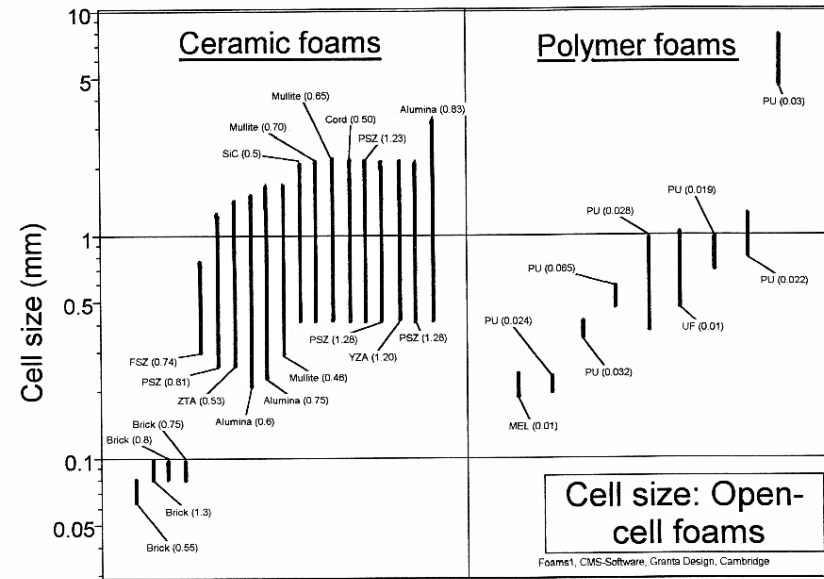
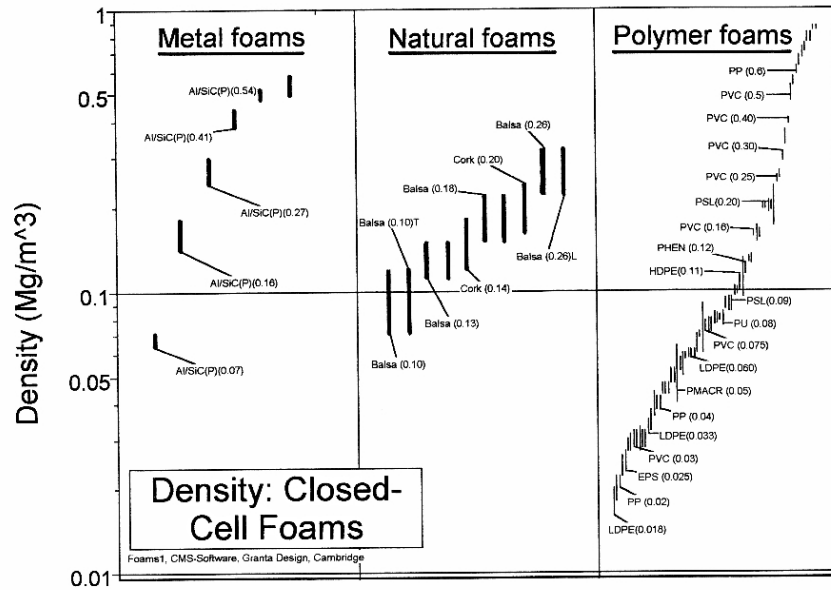


Thermal insulation applications;  
Usually a constraint on strength, too



May also have a constraint on  
maximum service temperature

Gibson, L. J., and M. F. Ashby. *Cellular Solids: Structure and Properties*. 2nd ed. Cambridge University Press, © 1997. Figures courtesy of Lorna Gibson and Cambridge University Press.



## Buoyancy

## Filtration and catalysis

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3.054 / 3.36 Cellular Solids: Structure, Properties and Applications  
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