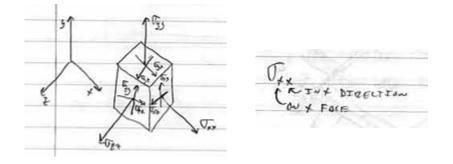
2.001 - MECHANICS AND MATERIALS I Lecture $\#\,13$ 10/25/2006 Prof. Carol Livermore

Recall from last time:

$$\begin{bmatrix} \sigma \end{bmatrix} = \begin{vmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{vmatrix}.$$

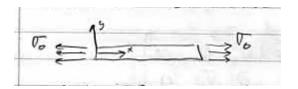
Diagonal terms are normal stresses. Off diagonal terms are shear stresses.



Not as bad as it seems:

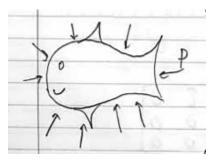
- 1. Linearity
- 2. Superposition

EXAMPLE: Uniaxial Stress



$$[\sigma] = \left| \begin{array}{ccc} \sigma_0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{array} \right|.$$

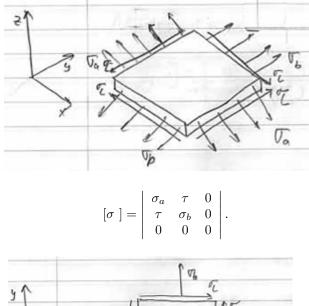
EXAMPLE: Hydrostatic Stress

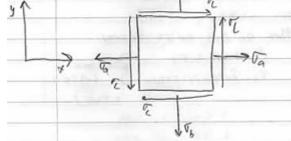


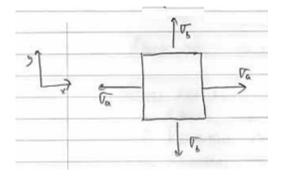
$$[\sigma] = \left| \begin{array}{ccc} -p & 0 & 0 \\ 0 & -p & 0 \\ 0 & 0 & -p \end{array} \right|.$$

Note: p is negative (compressive stresses are negative by convention)

EXAMPLE: Plane Stress

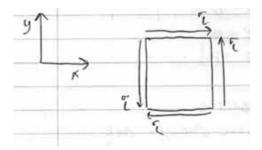






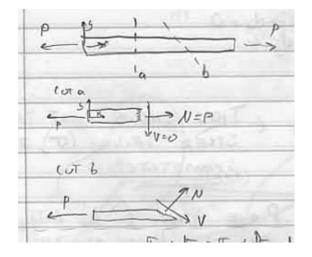
$$[\sigma] = \left| \begin{array}{ccc} \sigma_a & 0 & 0 \\ 0 & \sigma_b & 0 \\ 0 & 0 & 0 \end{array} \right|.$$

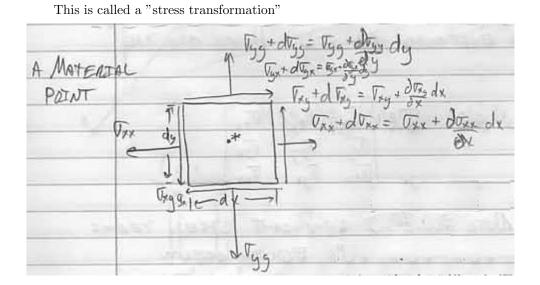
EXAMPLE: Shear Plane Stress



$$[\sigma] = \left| \begin{array}{ccc} 0 & \tau & 0 \\ \tau & 0 & 0 \\ 0 & 0 & 0 \end{array} \right|$$

Note: The stress at a material point that you see, and its magnitude, depends on the orientation of the coordinates relative to your loading. In other words: the state of stress is a function of the chosen coordinate system.





Equilibrium:

$$\sum F_x = 0$$
$$-\sigma_{xx} dy dz + (\sigma_x x + \frac{\partial \sigma_{xx}}{\partial x} dx) dy dz - \sigma_{yx} dx dz + (\sigma_{yx} \frac{\partial \sigma_{yx}}{\partial y} dx dy dz = 0$$

So:

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y}$$
$$\sum_{y} F_{y} = 0$$
$$\frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{xy}}{\partial x}$$

$$\sum M$$

$$(\sigma_{xy} + \frac{\partial \sigma_{xy}}{\partial x} dx) \frac{dx}{2} dy dz + \sigma_{xy} dy dz \frac{dx}{2} - \sigma_{yx} dx dz \frac{dy}{2} - (\sigma_{yx} + \frac{\partial \sigma_{yx}}{\partial y} dy) dx dz \frac{dy}{2} = 0$$

$$\sigma_{xy} - \sigma_{yx} + \frac{\partial \sigma_{xy}}{\partial x} \frac{dx}{2} - \frac{\partial \sigma_{yx}}{\partial y} \frac{dy}{2} = 0$$

For $dx, dy \to 0$:

$$\sigma_{xy} = \sigma_{yx}$$

This shows that the stress tensor (σ) is symmetric.

This was derived in plane stress (2-D) but it can be extended to 3-D. Here are the results:

So:

$$\begin{aligned}
\sigma_{xy} &= \sigma_{yx} \\
\sigma_{yz} &= \sigma_{zy} \\
\sigma_{xz} &= \sigma_{zx}
\end{aligned}$$

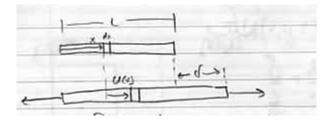
$$\begin{bmatrix}
\sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\
\sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\
\sigma_{zx} & \sigma_{zy} & \sigma_{zz}
\end{bmatrix},$$

S

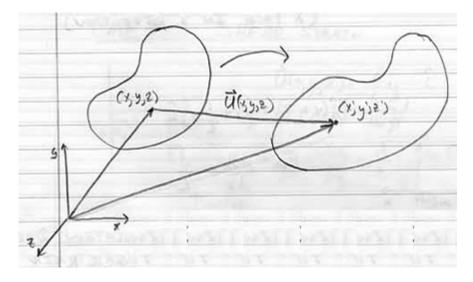
Note: 6 independent stress terms due to equilibrium. The stress tensor is symmetric.

Strain:

Uniaxial:

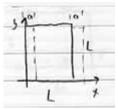


$$\epsilon(x) = \frac{du(x)}{dx}$$
$$\epsilon = \frac{\delta}{L}$$



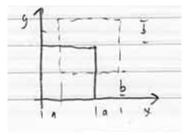
$$\vec{u}(x,y,z) = u_x(x,y,z)\hat{i} + u_y(x,y,z)\hat{j} + u_z(x,y,z)\hat{k}$$

Case 1:



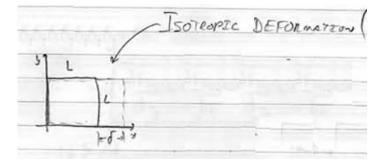
$$\vec{u}(x,y,z) = a\hat{i}$$

No strain. Rigid body translation. Case 2:



 $\vec{u}9x, y, z) = a\hat{i} + b\hat{j}$

No strain. Rigid body translation. Case 3:



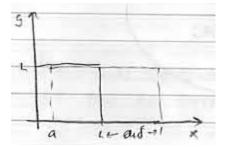
Isotropic Deformation: Stentches evenly so this is linear.

$$\vec{u}(x,y,z) = \frac{\delta x}{L}\hat{i}$$
$$\frac{du_x}{dx} = \frac{\delta}{L}$$

Define:

$$\epsilon_{xx} = \frac{du_x}{dx}$$
, Normal Strain (x face in x direction)

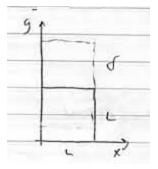
Case 4:



$$ec{u}(x,y,z) = \left(a + rac{\delta}{L}x
ight)\hat{i}$$
 $\epsilon_{xx} = rac{du_x}{dx} = rac{\delta}{L}$

Note: Rigid body translation does not effect the strain.

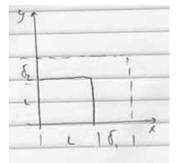
Case 5:



$$\vec{u}(x,y,z) = \frac{\delta}{L}y\hat{j}$$

$$\epsilon_{yy} = \frac{du_y}{dy} = \frac{\delta}{L}$$

Case 6:



$$\vec{u}(x, y, z) = \frac{\delta_1}{L}x\hat{i} + \frac{\delta_2}{L}y\hat{j}$$
$$\epsilon_{xx} = \frac{du_x}{dx} = \frac{\delta_1}{L}$$
$$\epsilon_{yy} = \frac{du_y}{dy} = \frac{\delta_2}{L}$$

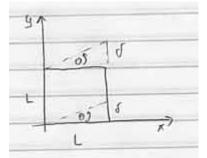


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$$\begin{split} \vec{u}(x,y,z) &= \frac{\delta}{L}y\hat{j}\\ \frac{\partial u_x}{\partial y} &= \frac{\delta}{L} = \tan\theta \approx \theta \end{split}$$

Define:

$$\gamma_{xy} = \theta$$



$$\vec{u}(x, y, z) = \frac{\delta}{L}x\hat{j}$$
$$\frac{\partial u_y(x)}{\partial x} = \frac{\delta}{L} = \theta$$
$$\gamma_{yx} = \theta$$
$$\gamma_{yx} = \frac{du_x}{dy} + \frac{du_y}{dx}$$

Define:

$$\epsilon_{xy} = \epsilon_{yx} = \frac{1}{2} \left[\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right]$$