## 2.001 - MECHANICS AND MATERIALS I Lecture #2612/11/2006 Prof. Carol Livermore

Energy Methods

3 Basic Ingredients of Mechanics:

- 1. Equilibrium
- 2. Constitutive Relations  $\sigma - \epsilon \dots$  Stress-Strain  $F - \delta$  Force-Deformation
- 3. Compatibility Dealing with geometric considerations

Castigliano's Theorem

Start with work:

$$W = \int \vec{F} \cdot d\vec{s}$$



Conservative Forces: EX: Gravity



 $u=mgh \Rightarrow \,$ Potential Energy, Path Independent

$$W = \int \vec{F} \cdot d\vec{s} = \int_0^h mgdz = mgh$$

Note: Elastic systems are conservative. Plastic deformation is *not* conservative.

EX: Springs



Energy =  $1/2k\delta^2$ 

$$W = \int_0^\delta P d\delta = \int_0^\delta k \delta d\delta = \frac{1}{2} k \delta^2$$



Stored Energy = Work Put In

U = W

What if the spring were stretched a little further?



Complementary Energy  $(U^*)$ 



$$U^* = \int \delta dP$$

Note:  $U = U^*$  due to linearity



 $U \neq U^*$  if this is non-linear

What if the load were stretched a little further?



$$dU^* = \delta dP$$
$$\delta = \frac{dU^*}{dP}$$

Recall, for linear elastic material

$$\delta = \frac{dU}{dP}$$

Castigliano's Theorem:

Express complementary energy in terms of the loads

Add up all the complementary energy stroed in all the pieces

Find displacement of given point from derivative of  $U^\ast$  with respect to P at that point in that direction

Example: Linear Spring

$$U^{*} = \int \delta dP = \int \frac{P}{k} dP = \frac{P^{2}}{2k} = \frac{k^{2} \delta^{2}}{2k} = \frac{1}{2} k \delta^{2}$$

Example: Springs in series

$$F_1 = F_2 = P$$

$$U = \sum_{i} U_{i} = \frac{F_{1}^{2}}{2k_{1}} + \frac{F_{2}^{2}}{2k_{2}} = \frac{P^{2}}{2k_{1}} + \frac{P^{2}}{2k_{2}}$$

Use Castigliano's Theorem

$$\delta = \frac{U^*}{dP} = \frac{P}{k_1} + \frac{P}{k_2}$$

## Find $\delta_1$ using Castigliano's Theorem Put a fictitous $P_f$ to coinside with $\delta_1$



$$\sum F_x = 0$$

$$-F_1 + P_f + P = 0 \Rightarrow F_1 = P_f + P$$

$$-F_2 + P = 0 \Rightarrow F_2 = P$$

$$U = \frac{F_1^2}{2k_1} + \frac{F_2^2}{2k_2} = \frac{(P_f + P)^2}{2k_1} + \frac{P^2}{2k_2}$$

$$\delta_1 = \frac{\partial U}{\partial P_f} = \frac{P_f + P}{k_1}$$

Recall  $P_f = 0$ , so:

$$\delta_1 = \frac{P}{k_1}$$
$$\delta = \frac{dU}{dP} = \frac{P_f + P}{k_1} + \frac{P}{k_2}$$
$$P_f = 0$$

So:

$$\delta = \frac{P}{k_1} + \frac{P}{k_2}$$

Note: This was done without doing compatibility explicitly. Example Truss



"K= EA"		KAO- EA	Ker = EA
per -L	1040	Lsino	L

$$U = \sum_{i} U_{i} = \frac{F_{AB}^{2}}{2k_{AB}} + \frac{F_{BC}^{2}}{2k_{BC}}$$

Equilibrium of B



$$\sum F_x = 0$$
$$F_{AB} - F_{BC} \sin \theta = 0$$
$$\sum F_y = 0$$
$$-P - F_{BC} \cos \theta = 0$$
$$P = -F_{BC} \cos \theta$$
$$F_{BC} = \frac{-P}{\cos \theta}$$
$$F_{AB} = P \tan \theta$$

$$\begin{split} U &= \frac{(P \tan \theta)^2}{2k_{AB}} + \left(\frac{P}{\cos \theta}\right)^2 \frac{1}{2k_{BC}} \\ &- u_y^B = \frac{dU}{dP} = \frac{P \tan^2 \theta}{k_{AB}} + \frac{P}{\cos^2 \theta k_{BC}} \end{split}$$

Strain Energy Density

$$W = \int F d\delta$$
$$u = \int \sigma d\epsilon$$

This is useful in beam bending.

Stored Energy in A Beaam  $(\sigma_{xx}, \epsilon_{xx})$ 

Total Energy Stored

$$U = \int_{V} dV \int_{0}^{\epsilon} \sigma_{xx} d\epsilon_{xx}$$

Recall:

For a beam:

$$\sigma_{xx} = E\epsilon_{xx}$$

For one material:

$$\sigma_{xx} = \frac{-My}{I}$$

Beam:

$$U = \int_{V} dV \int_{\epsilon} \sigma_{xx} d\epsilon_{xx}$$
$$= \int_{V} dV \int_{0}^{\sigma_{xx}} \frac{\sigma_{xx} d\sigma_{xx}}{E}$$
$$= \int_{V} dV \frac{\sigma_{xx}^{2}}{2E}$$

For one material:



$$U = \int_V \frac{M(x)^2}{2EI^2} y^2 dV$$

So:

$$U = \frac{1}{2EI} \int_{a} M(x)^2 dx$$
 For special case of one material beam.

Example:



$$M(x) = -P(L-x)$$
$$U = \frac{1}{2EI} \int_0^L P^2(L-x)^2 dx = \frac{P^2 L^3}{6EI}$$
$$\delta_{tip} = \frac{dU}{dP} = \frac{PL^3}{3EI}$$